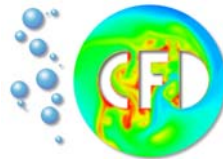


A Newton – Like Finite Element Solver for Compressible Particle – Laden Gas Flows

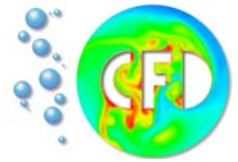
Marcel Gurriss¹, Dmitri Kuzmin², Stefan Turek¹

Dortmund University of Technology¹

University of Erlangen²



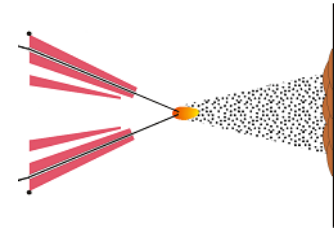
marcel.gurriss@math.uni-dortmund.de



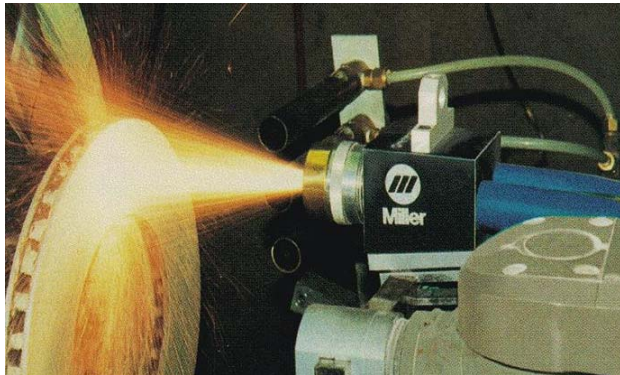
Aims

- Simulation of the gas-particle in arc spraying equipment
- High-resolution (semi-) implicit FEM-TVD schemes
- Stationary solutions

Experimental setup



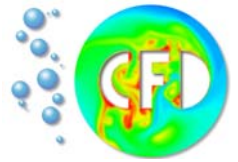
Brake disk coating



Contents

- FEM discretization
- Semi-implicit pseudo time stepping and Newton-like schemes
- Boundary conditions
- Preconditioner
- Numerical results

The 2 – Fluid Model



Gas phase:

$$\partial_t \begin{bmatrix} \alpha_g \rho_g \\ \alpha_g \rho_g \mathbf{u}_g \\ \alpha_g \rho_g E_g \end{bmatrix} + \nabla \cdot \begin{bmatrix} \alpha_g \rho_g \mathbf{u}_g \\ \alpha_g \rho_g \mathbf{u}_g \otimes \mathbf{u}_g + \alpha_g \mathbf{I} P \\ \alpha_g \mathbf{u}_g (\rho_g E_g + P) \end{bmatrix} = \begin{bmatrix} 0 \\ -\mathbf{F}_D \\ -\mathbf{u}_p \cdot \mathbf{F}_D - Q_T \end{bmatrix}$$

Particulate phase:

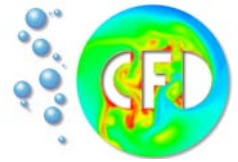
$$\partial_t \begin{bmatrix} \alpha_p \rho_p \\ \alpha_p \rho_p \mathbf{u}_p \\ \alpha_p \rho_p E_p \end{bmatrix} + \nabla \cdot \begin{bmatrix} \alpha_p \rho_p \mathbf{u}_p \\ \alpha_p \rho_p \mathbf{u}_p \otimes \mathbf{u}_p \\ \alpha_p \rho_p \mathbf{u}_p E_p \end{bmatrix} = \begin{bmatrix} 0 \\ \mathbf{F}_D \\ \mathbf{u}_p \cdot \mathbf{F}_D + Q_T \end{bmatrix}$$

Saturation condition:

$$\alpha_g + \alpha_p = 1$$

- Two-way coupling via volume fractions and interfacial forces

High – Resolution Schemes



High – order scheme:

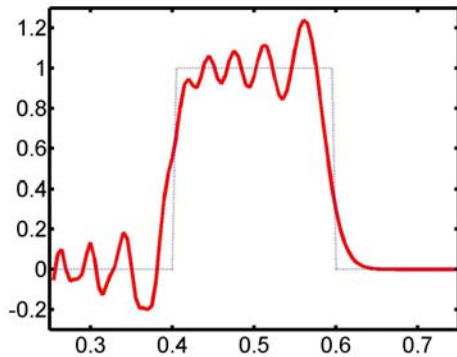
$$M_C \frac{dU}{dt} = KU$$



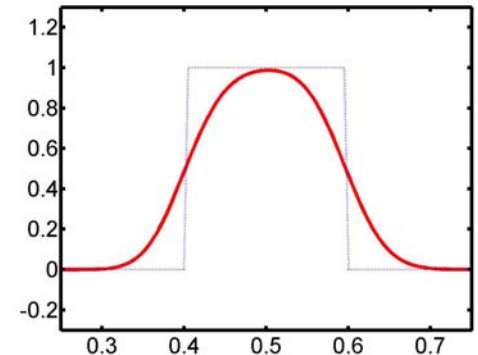
Low – order scheme:

$$M_L \frac{dU}{dt} = KU + DU = LU$$

- Oscillatory
- Second order

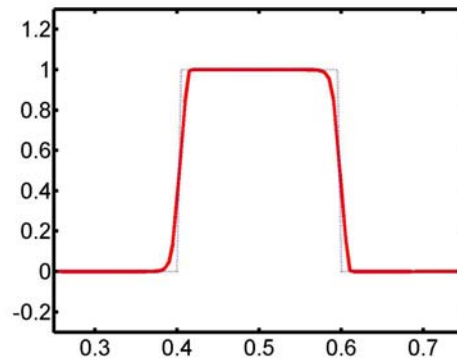


- Non – oscillatory
- First order

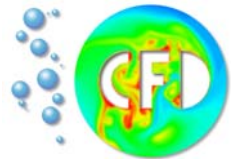


High – resolution scheme:

$$M_L \frac{dU}{dt} = KU + DU + F^*U = K^*U$$



- Non - oscillatory
- Less diffusive
- Variable order



Mass lumping:

$M_C S$



$M_L S$

Douglas – Rachford splitting

$$M_L \frac{\tilde{U} - U^n}{\Delta t} = \tilde{F} + M_L S^n$$
$$\frac{U^{n+1} - \tilde{U}}{\Delta t} = S^{n+1} - S^n$$

- Time step independent steady–state solutions
- Restrictive time step constraints
- Slow convergence

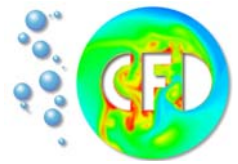


Strongly coupled strategy

$$M_L \frac{U^{n+1} - U^n}{\Delta t} = F^{n+1} + M_L S^{n+1}$$

- Time step independent steady–state solutions
- No time step constraints
- Fast convergence

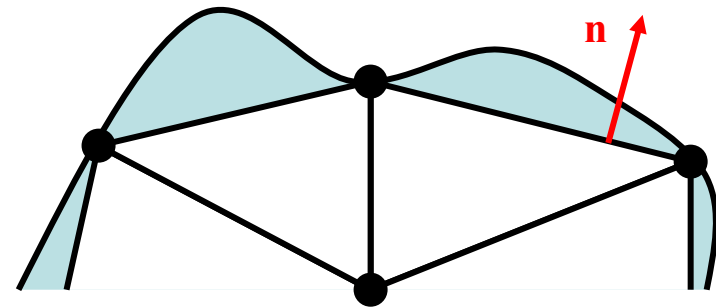
Weak Neumann – Type Boundary Conditions



Integration by parts:

$$\sum_j m_{ij} \frac{dU_j}{dt} = \sum_j \mathbf{c}_{ji} \cdot \mathbf{F}_j - \int_{\partial\Omega} \varphi_i \mathbf{n} \cdot \mathbf{F}_h ds, \quad \forall i$$

- Implicit treatment possible
- Unconditionally stable
- Boundary conditions locally satisfied



$$\int_{\partial\Omega} \varphi_i \mathbf{n} \cdot \mathbf{F}_h ds$$

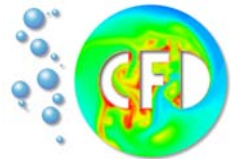


Evaluation of the boundary flux by solution of a boundary Riemann problem



$$\int_{\partial\Omega} \varphi_i \mathbf{n} \cdot \tilde{\mathbf{F}}_h ds$$

Boundary Flux & Boundary Integral

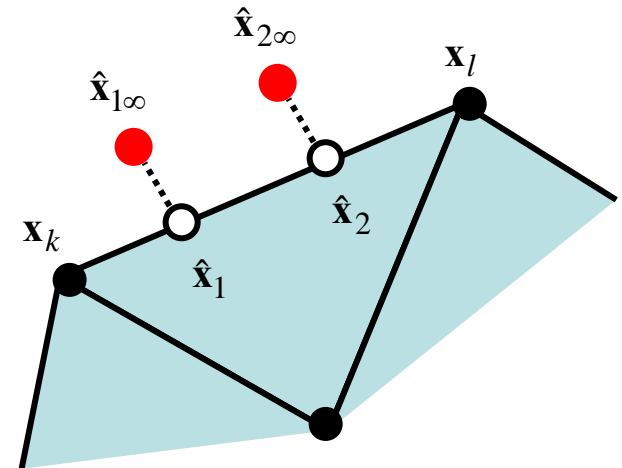


Evaluation of the boundary integral:

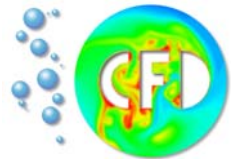
- Ghost nodes
- Edgewise integration

Roe flux:

$$F_{i\infty} = \frac{F_i + F_\infty}{2} - \frac{1}{2} |A_{i\infty}| (U_\infty - U_i)$$



- Consistent with interior discretization
- U_∞ defined by the Riemann invariants
- Boundary conditions for incoming Riemann invariants

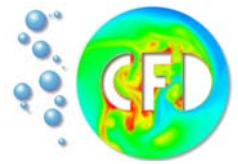


Euler equations:

- Mirror condition:
$$\begin{aligned}\rho_\infty &= \rho_i \\ u_{\tau\infty} &= u_{\tau i} \\ u_{n\infty} &= -u_{ni} \\ E_\infty &= E_i\end{aligned}\quad \mathbf{u} = u_n \mathbf{n} + u_\tau \boldsymbol{\tau}$$

2 – Fluid Model:

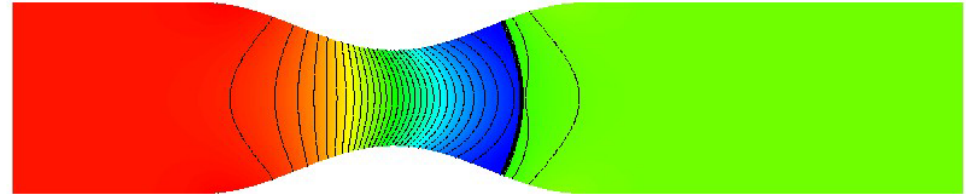
- Penalty term:
$$penalty = -\sigma \int_{\Gamma_{wall}} \varphi |u_n| \rho^2 u_n \mathbf{n} ds$$
- Addition of penalty terms to the momentum equations of both phases
- Optional elimination of normal fluxes in the boundary integral



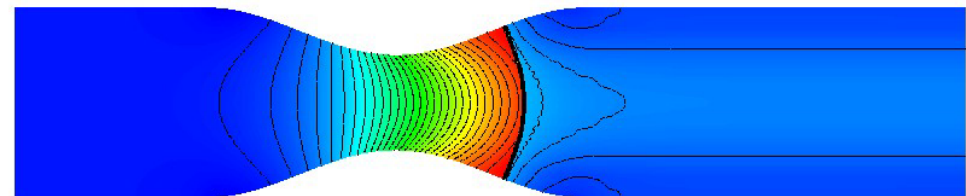
Nozzle with „pressure - outlet“:

- Subsonic inlet and outlet
- Outlet pressure: $P_{out} = 2/3$
- Convergence

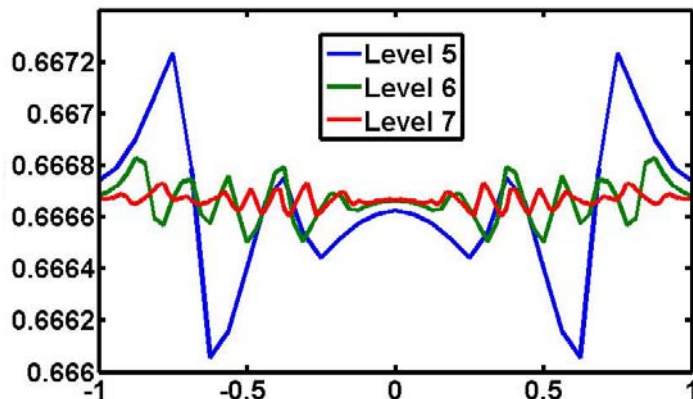
Pressure (red: $P=1$, blue: $P=0.13$)



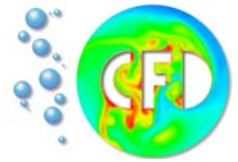
Mach number (red: $M=2.03$, blue: $M=0.27$)



Computed outlet pressure



Convergence Analysis: „Pressure – Outlet“



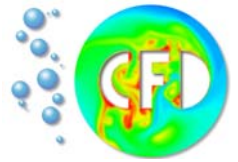
Outlet pressure:

Level	NVT	NEL	NVT ^{out}	E ₂ ^{out}	p ^{out}
5	5313	5120	33	2.50 · 10 ⁻³	1.32
6	20865	20480	65	1.00 · 10 ⁻³	1.12
7	82689	81920	129	4.62 · 10 ⁻⁴	

$$E_2^{out} = \frac{\|P_h - P_{out}\|_{2,\Gamma_{out}}}{\|P_{out}\|_{2,\Gamma_{out}}}$$

$$p^{out} = \frac{\log\left(\frac{\|P_h - P_{out}\|_{2,\Gamma_{out}}}{\|P_{h/2} - P_{out}\|_{2,\Gamma_{out}}}\right)}{\log(2)}$$

Implicit Solver & Newton's Method



Backward Euler scheme:

$$M_L \frac{U^{n+1} - U^n}{\Delta t} = (F + S)^{n+1}$$

Taylor series:

$$(F + S)^{n+1} = (F + S)^n + \left(\frac{\partial(F + S)}{\partial U} \right)^n (U^{n+1} - U^n) + O\left(\|U^{n+1} - U^n\|^2\right)$$

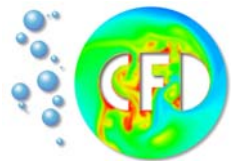
Semi – implicit scheme:

$$\left[\frac{M_L}{\Delta t} - \left(\frac{\partial(F + S)}{\partial U} \right)^n \right] (U^{n+1} - U^n) = (F + S)^n$$

Newton's method:

$$-\left(\frac{\partial(F + S)}{\partial U} \right)^n (U^{n+1} - U^n) = F^n + S^n$$

- Omitting the lumped mass matrix yields Newton's method
- Second order convergence if F sufficiently smooth



$$F_i = \sum_j^{\text{low}} \mathbf{c}_{ji} \cdot \mathbf{F}_j - B_i + D_{ij} (U_j - U_i)$$

Fluxes:

- Low – order approximation
- Parameter – free
- Increased robustness due to improved matrix properties



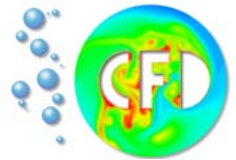
$$\frac{\partial F_i^{\text{low}}}{\partial U_j} \approx \mathbf{c}_{ji} \cdot \frac{\partial \mathbf{F}_j}{\partial U_j} - \frac{\partial B_i}{\partial U_j} + D_{ij}$$

$$B_i = \int_{\partial\Omega} \varphi_i \mathbf{n} \cdot \mathbf{F}_h ds$$

Source terms:

- Linearization
- Non – smooth terms are assumed constant
- Jacobian known analytically

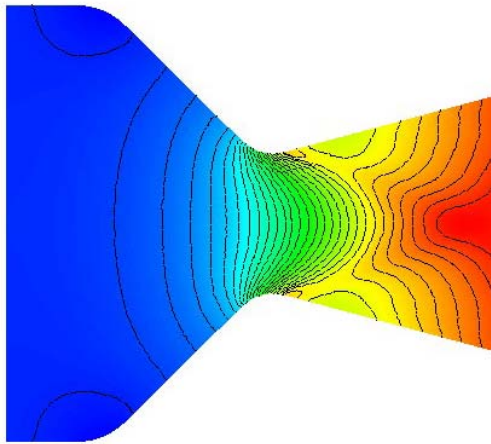
2-Fluid Model



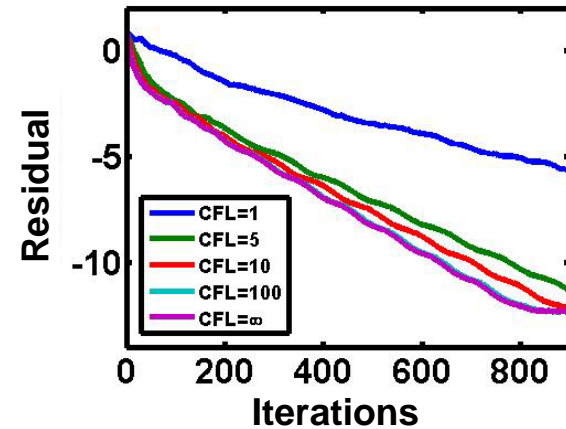
Nozzle flow:

- Subsonic inlet, supersonic outlet
- Wide range of Mach numbers
- Convergence to steady – state

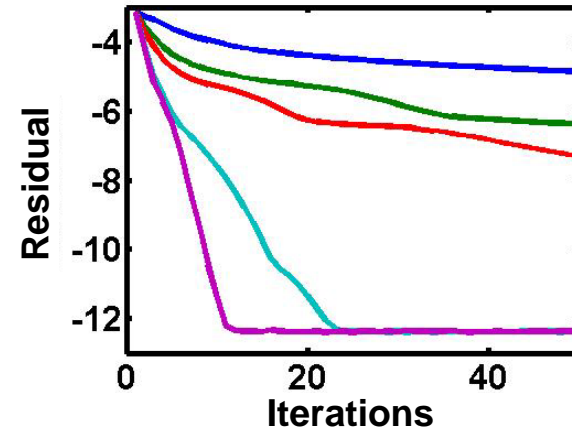
Mach number (blue, $M=0.1$, red: $M=2.22$)

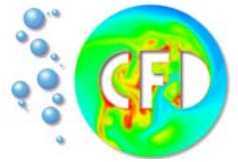


High – resolution scheme



Low – order scheme





Conclusions

- High - resolution FEM – TVD scheme
- Stationary solutions
- Wide range of Mach numbers
- Newton – like iterative solver
- Unconditional stability
- Improved boundary conditions
- Gain of efficiency due to strongly coupled strategy

Outlook

- Adaptivity
- Nonlinear multigrid
- 3D extension